

# Navigation and Orbit Phasing of Modular Spacecraft for Segmented Telescope Assembly about Sun-Earth L2

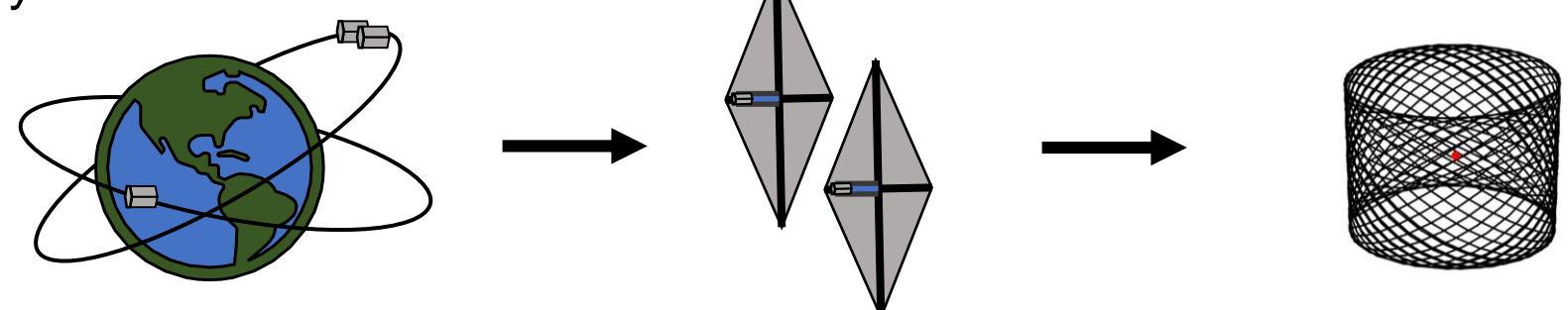
Gabriel Soto<sup>a,b</sup>, Dmitry Savransky<sup>a,b</sup>, Erik Gustafson<sup>a</sup>, Jacob Shapiro<sup>a,b</sup>, Dean Keithly<sup>a,b</sup>, Christopher Della Santina<sup>a</sup>

<sup>a</sup> Sibley School of Mechanical and Aerospace Engineering, Cornell University, Ithaca, NY, United States

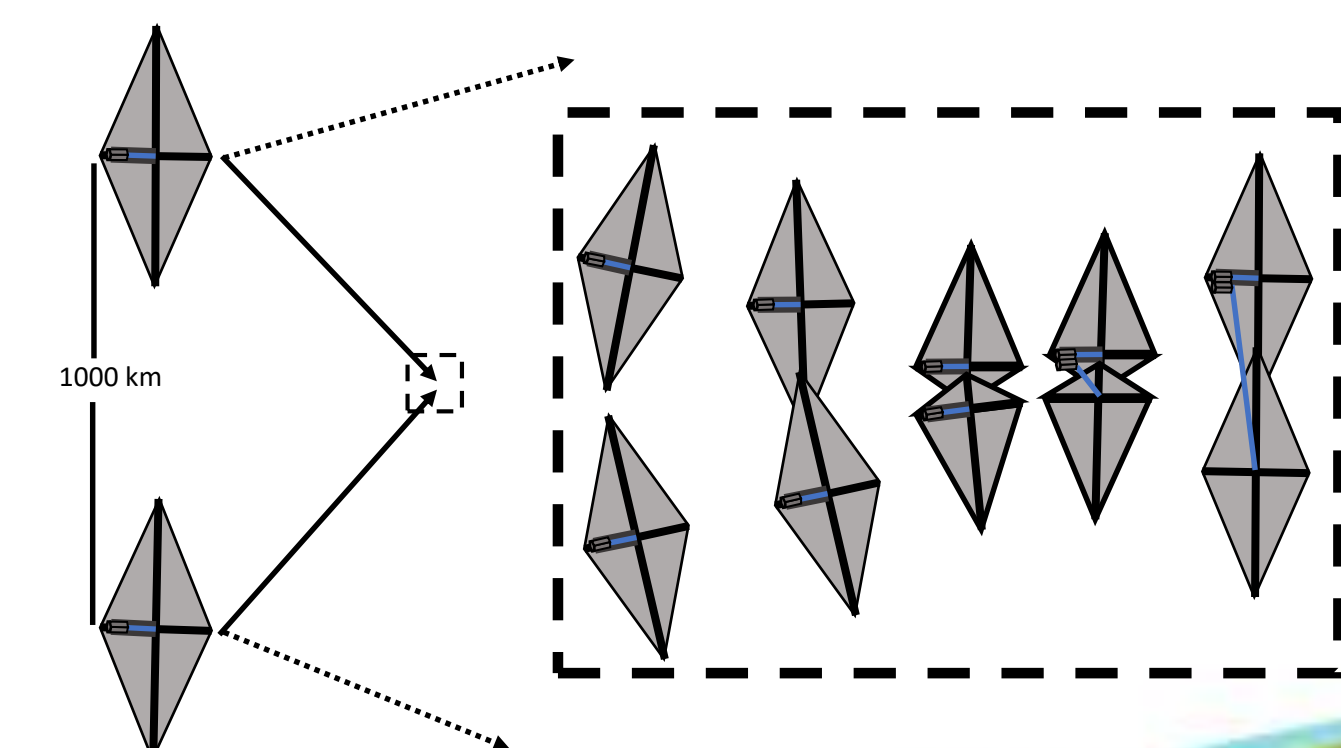
<sup>b</sup> Carl Sagan Institute, Ithaca, NY, United States



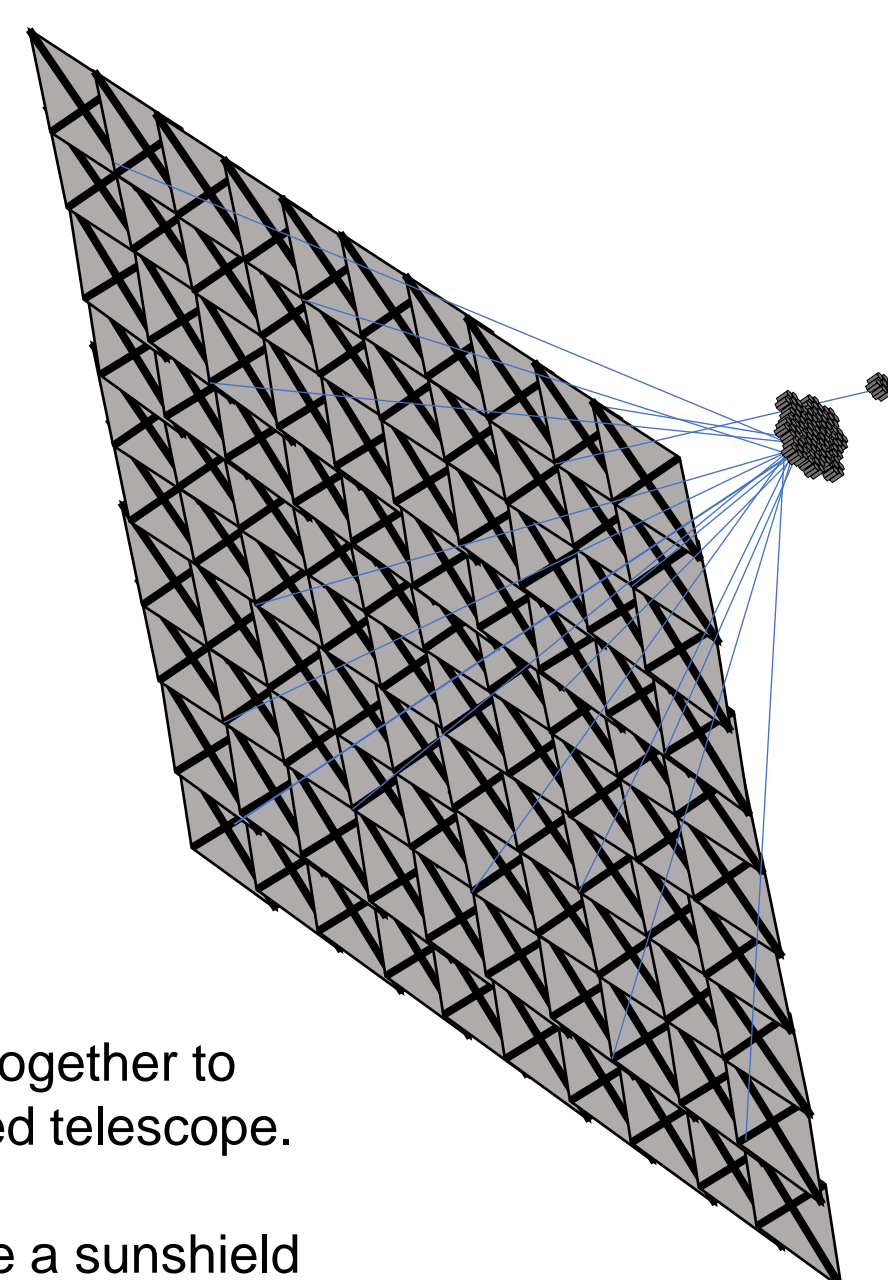
Modular spacecraft start on Earth orbits with mirror as payload.



- When within 1000 km, two spacecraft will rendezvous and dock together.
- Sails overlap, remain attached to mirror cluster through extensible tether.



- Mirrors all dock together to form a segmented telescope.
- Solar sails create a sunshield for the telescope.



- Dynamics are modeled using the Circular Three Body formalism<sup>1</sup>.
- Solar radiation pressure exerts specific force onto each solar sail<sup>2</sup>.

$$\mathbf{a}_s = \beta \frac{1-\mu}{r_1^2} (\hat{\mathbf{r}}_1 \cdot \hat{\mathbf{n}})^2 \hat{\mathbf{n}} \quad \beta = \frac{\sigma^*}{\frac{m_p}{A} + \sigma_s}$$

$$\hat{\mathbf{n}} = \cos(\alpha) \cos(\delta) \hat{\mathbf{x}} + \sin(\alpha) \cos(\delta) \hat{\mathbf{y}} + \sin(\delta) \hat{\mathbf{z}}$$

- The lightness number  $\beta$  is used as a non-dimensionalized sail characteristic acceleration.
- It is a function of the sail area  $A$ , payload mass  $m_p$ , sail areal density  $\sigma_s$  of units  $\frac{g}{m^2}$  and a critical lightness number  $\sigma^*$ .

## 1 Earth Escape

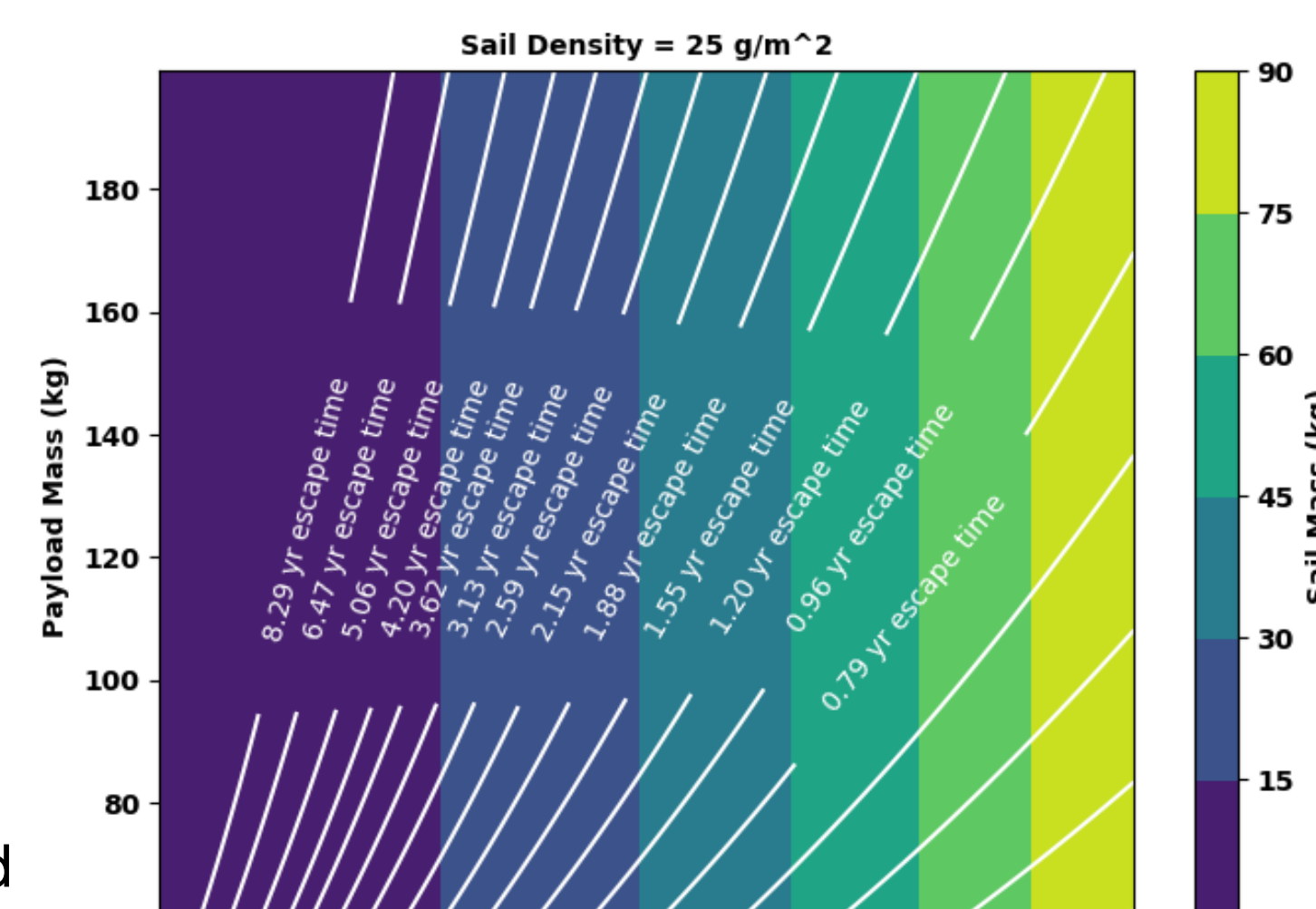
- A control law<sup>3</sup> for the sail angles is used to maximize energy gain:

$$n_x = \frac{|v_y|}{\sqrt{v_y^2 + \xi^2(v_y^2 + v_z^2)}} \max_{\hat{\mathbf{n}}} \mathbf{a}_s \cdot \mathbf{v}$$

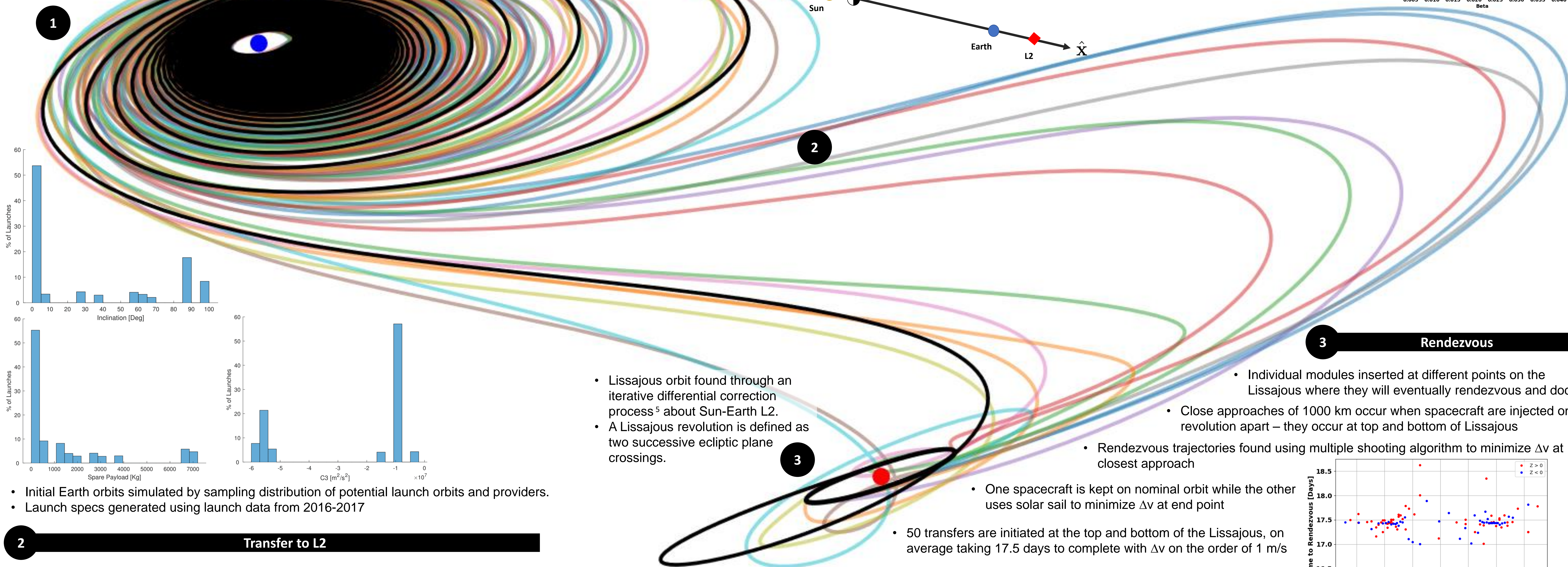
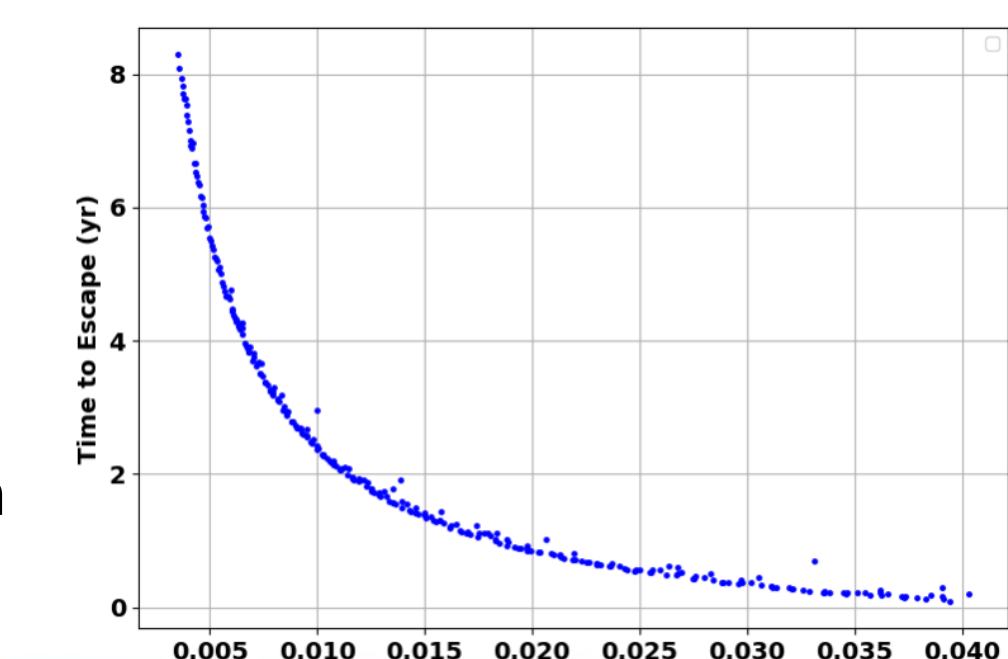
$$n_y = \xi n_x$$

$$n_z = \frac{v_z}{v_y} n_y \quad \xi = \frac{-3v_x v_y \pm v_y \sqrt{9v_x^2 + 8(v_y^2 + v_z^2)}}{4(v_y^2 + v_z^2)}$$

- Equations of motion with sail normal control law integrated until escape energy is reached



- Assuming a set sail density based on JPL NEA Scout design
- Design space includes payload mass and sail size – each corresponds to a characteristic acceleration
- Time to escape earth orbit shown as contours on design space plot



- Lissajous orbit found through an iterative differential correction process<sup>5</sup> about Sun-Earth L2.
- A Lissajous revolution is defined as two successive ecliptic plane crossings.

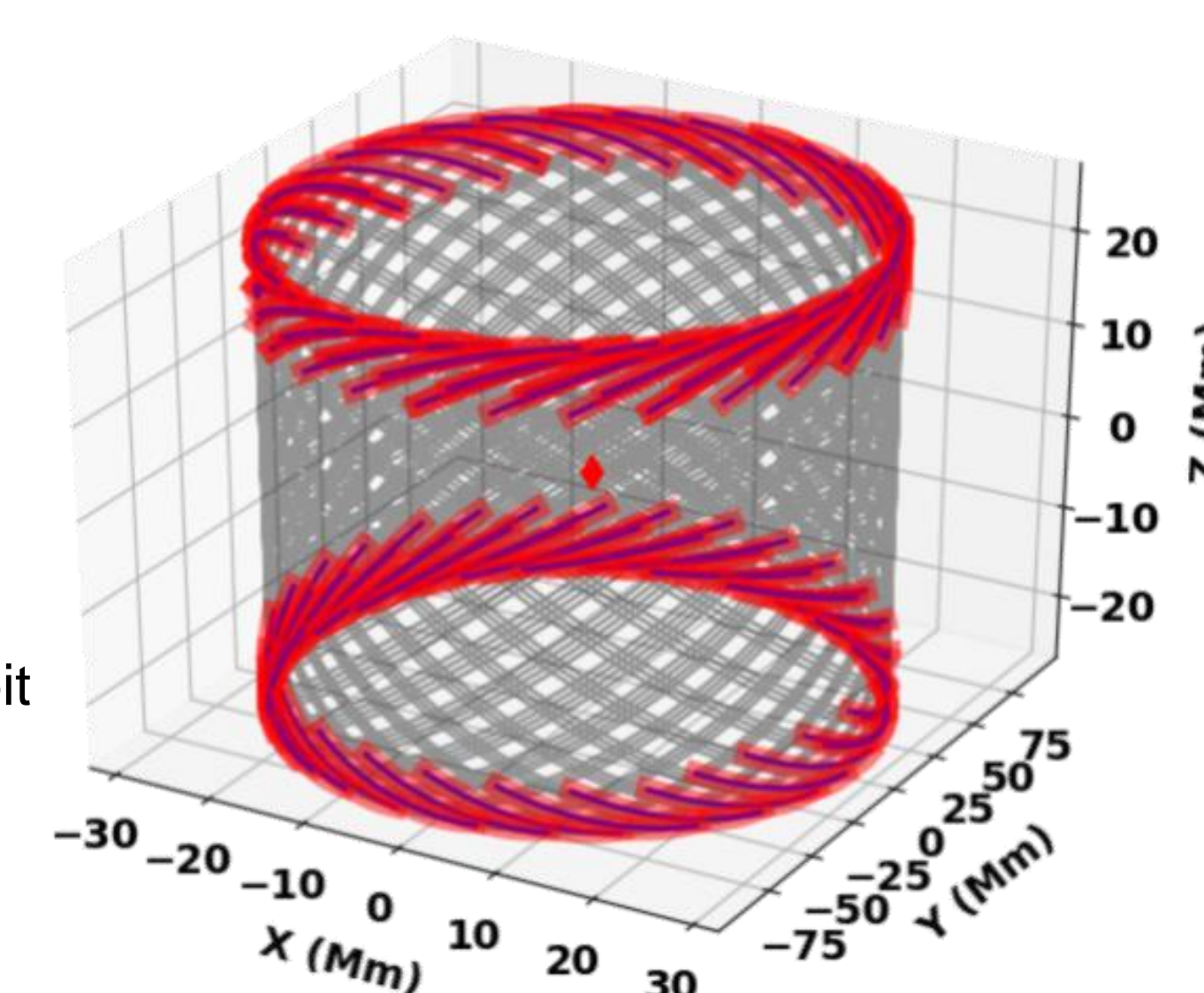
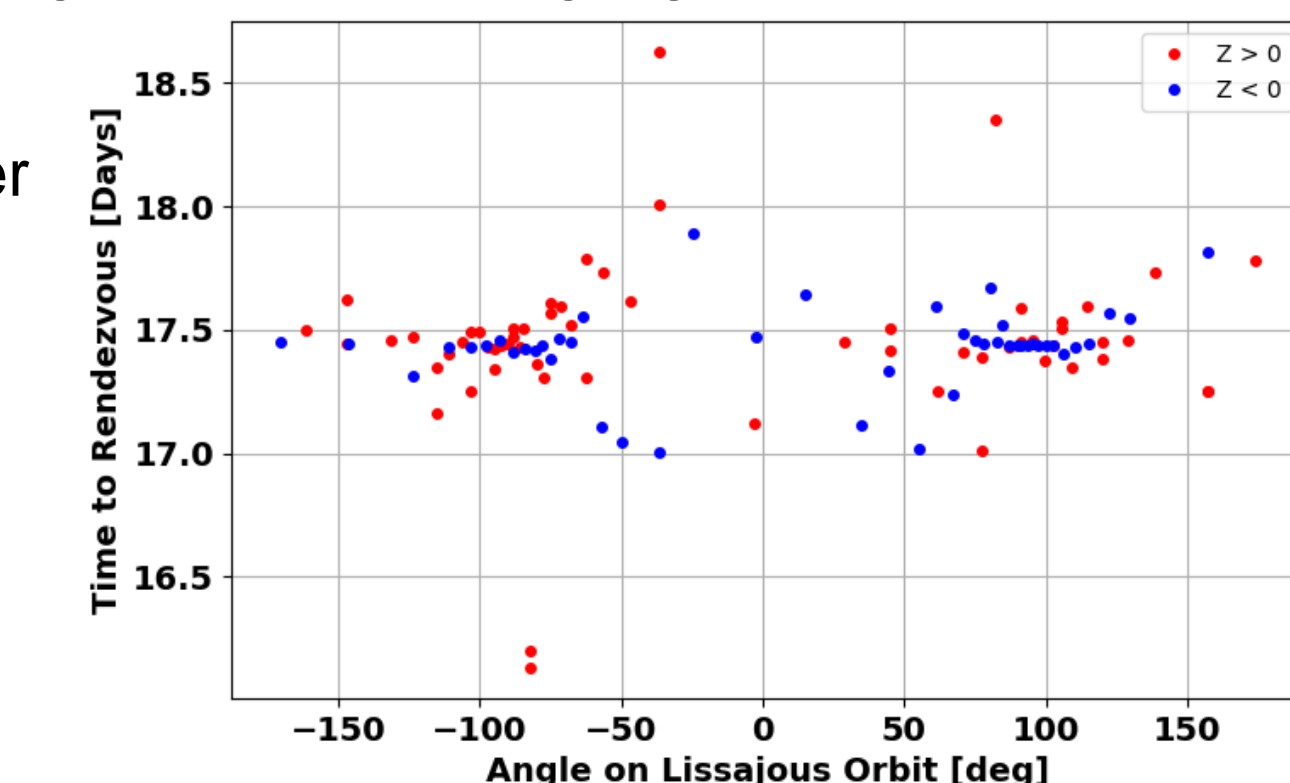
## 3 Rendezvous

- Individual modules inserted at different points on the Lissajous where they will eventually rendezvous and dock
- Close approaches of 1000 km occur when spacecraft are injected one revolution apart – they occur at top and bottom of Lissajous

- Rendezvous trajectories found using multiple shooting algorithm to minimize  $\Delta v$  at closest approach

- One spacecraft is kept on nominal orbit while the other uses solar sail to minimize  $\Delta v$  at end point

- 50 transfers are initiated at the top and bottom of the Lissajous, on average taking 17.5 days to complete with  $\Delta v$  on the order of 1 m/s



## 2 Transfer to L2

- Transfer to L2 initiated sometime before or after reaching escape energy
- Constrained optimization problem using  $\mathbf{f}$ : equations of motion perturbed by  $\mathbf{a}_s$

$$H = J + \lambda \cdot \mathbf{f} \quad \dot{\lambda} = -\frac{\partial H}{\partial \mathbf{x}} \quad \frac{\partial H}{\partial \hat{\mathbf{n}}} = \mathbf{0}$$

Variational Hamiltonian: minimize cost  $J$  and constrained by equations of motion

Co-states add 6 more equations to integrate

Definition of new control law

- Boundary value problem with 12 variables, 6 boundary conditions each at start and end of trajectory (position and velocity)
- Single shooting problem wrapped into optimization problem using basinhopping algorithm
- Optimization variables:

$$[t_i, t_f, \Delta t, \lambda_{x_0}, \lambda_{y_0}, \lambda_{z_0}, \lambda_{v_{x,0}}, \lambda_{v_{y,0}}, \lambda_{v_{z,0}}]$$

- $t_i$  defines time at which transfer to L2 is initiated
- $t_f$  defines point where spacecraft is injected into Lissajous orbit

- Objective function integrates initial states augmented with Lagrange multipliers for  $\Delta t$  time

- Minimizes difference between desired final states and final result of integration

$$n_x = \frac{|\lambda_{v_y}|}{\sqrt{\lambda_{v_y}^2 + \xi^2(\lambda_{v_y}^2 + \lambda_{v_z}^2)}} \max_{\hat{\mathbf{n}}} \mathbf{a}_s \cdot \lambda_{\mathbf{v}}$$

$$n_y = \xi n_x$$

$$n_z = \frac{\lambda_{v_z}}{\lambda_{v_y}} n_y \quad \xi = \frac{-3\lambda_{v_x} \lambda_{v_y} \pm \lambda_{v_y} \sqrt{9\lambda_{v_x}^2 + 8(\lambda_{v_y}^2 + \lambda_{v_z}^2)}}{4(\lambda_{v_y}^2 + \lambda_{v_z}^2)}$$

## Acknowledgements and References

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Send correspondence to Gabriel Soto

